



# Compensating Calorimeters

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# Idea of compensation

- Smaller calorimeter response to non-em components of hadron showers than to em components
    - Reason: invisible energy  $\rightarrow$  no contribution to calorimeter signal
    - Main source: energy used to release nucleons from nuclei + myons + neutrinos (escape the detector)
  - Consequences of non-compensation:
    - Non-linearity of hadronic calorimeter response
    - Degradation of the energy resolution
    - Effects on the line shape of the hadronic calorimeter
- => Need to compensate for the invisible energy**

# Important definitions

- *Calorimeter response* = 
$$\frac{\text{average calorimeter signal}}{\text{energy of the particle}}$$
- Linear calorimeter:
  - average signal proportional to particle energy
  - response = constant as a function of energy (benchmark particles = mips)
- What does  $X/\text{mip} < 1$  mean?
  - on average, smaller signal for particles “X” of a given energy than for mips of the same energy
- *Sampling fraction* = 
$$\frac{\text{energy deposited by mips in the active calorimeter layer}}{\text{total energy deposited in the calorimeter}}$$

# The e/h value

- e/h value = degree of non-compensation in calorimeters
- Definition (as derived from e/π - measurements):

$$\frac{e}{h} = \frac{1 - f_{em}(E)}{\pi/e(E) - f_{em}(E)}$$

- With different shower particles that contribute to em and non-em components:

$$\frac{e}{h} = \frac{e/mip}{f_{rel} \cdot rel/mip + f_p \cdot p/mip + f_n \cdot n/mip}$$

- Compensation  $\Leftrightarrow e/h = 1$ 
  - Undercompensation  $\Leftrightarrow e/h > 1$
  - Overcompensation  $\Leftrightarrow e/h < 1$

# The $e/h$ value (2)

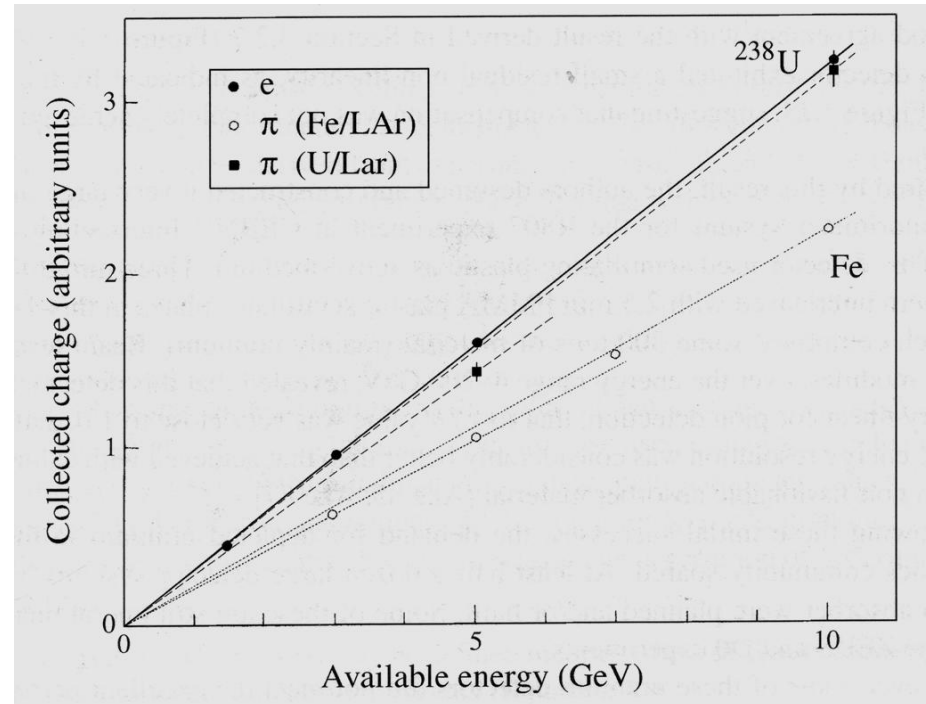
- In homogeneous calorimeters:
  - Always undercompensation,  $e/h > 1$ , since  $f_{\text{rel}} + f_p + f_n < 1$  due to the invisible energy
- In sampling calorimeters:
  - Tuning of parameters until  $e/h = 1$  is achieved.
  - Once active and passive materials have been chosen  $\rightarrow$  values of  $f_{\text{rel}}$ ,  $f_p$ ,  $f_n$  are fixed
  - $\text{rel/mip} = 1$

$\Rightarrow$  Only tuning of  $e/\text{mip}$ ,  $p/\text{mip}$  and  $n/\text{mip}$  possible

  - Usually: undercompensation,  $e/h > 1 \Rightarrow$  reduction

# The first compensating calorimeter

- First uranium calorimeter by Fabjan and Willis
- 250  $^{238}\text{U}$  plates (1.7mm thick) in liquid argon (20mm gaps between plates)
- Compensation almost achieved  
→  $e/h \sim 1.1-1.2$



- Electron measurements as normalization
- Small non-linearities

# Experimental insights from first experiments

- Non-linearities:
  - Undercompensating calorimeters:  
Increase of hadronic response with increasing energy
  - Overcompensating calorimeters:  
Decrease of hadronic response with increasing energy
- Material choices:
  - For a certain passive material: For compensation, need the right active material in the right proportion.
- 3 different methods to achieve compensation:
  - Reduction of the em response
  - Boosting the non-em response
  - Off-line compensation

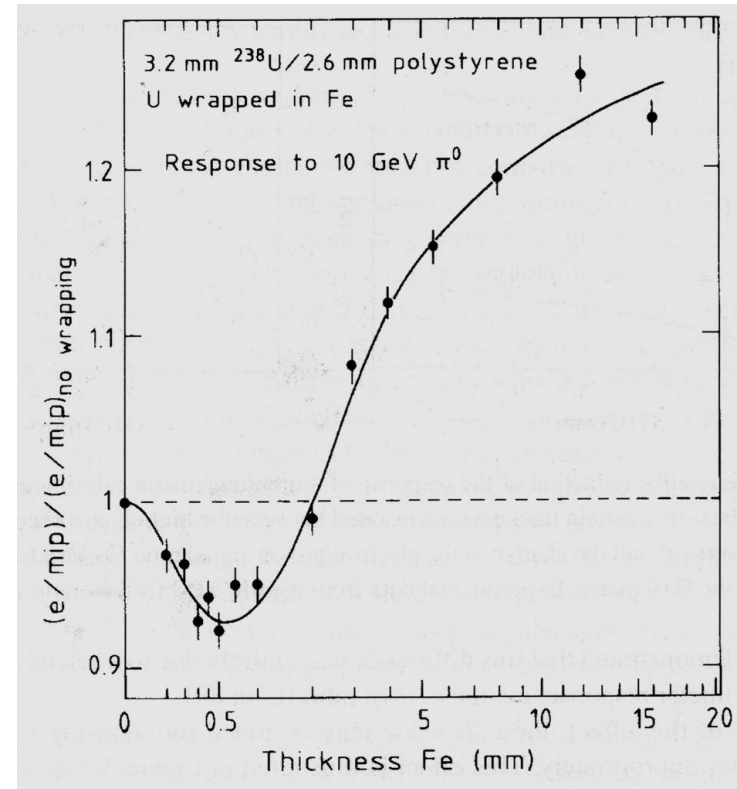


# Reducing the em response

- Choose high-Z absorber material, e.g. lead, uranium →  
 $e/mip = 0.6-0.7$   
=> Ideally compensate 30-40% of invisible energy
  - Reason for suppression of em response in sampling calorimeters with high-Z absorber material:
    - Dominating contribution of photoelectric effect to cross section
    - Contribution of created photoelectron to calorimeter signal  
<=> interaction takes place very close to the boundary layer
- => Photoelectron can escape into the active material => signal

# Reducing the em response (2)

- Further suppression of  $e/mip$ :  
shielding the active layers with thin sheets of passive low-Z material (e.g. iron foil)
- $e/mip \rightarrow$  function of thickness of these foils
- ZEUS experiment:  
uranium plates wrapped in stainless steel



- Minimum:  $\sim 500\mu\text{m}$  iron foil  $\approx$  range of electron with  $\sim 700\text{keV}$  (= energy where photoeffect starts dominating)

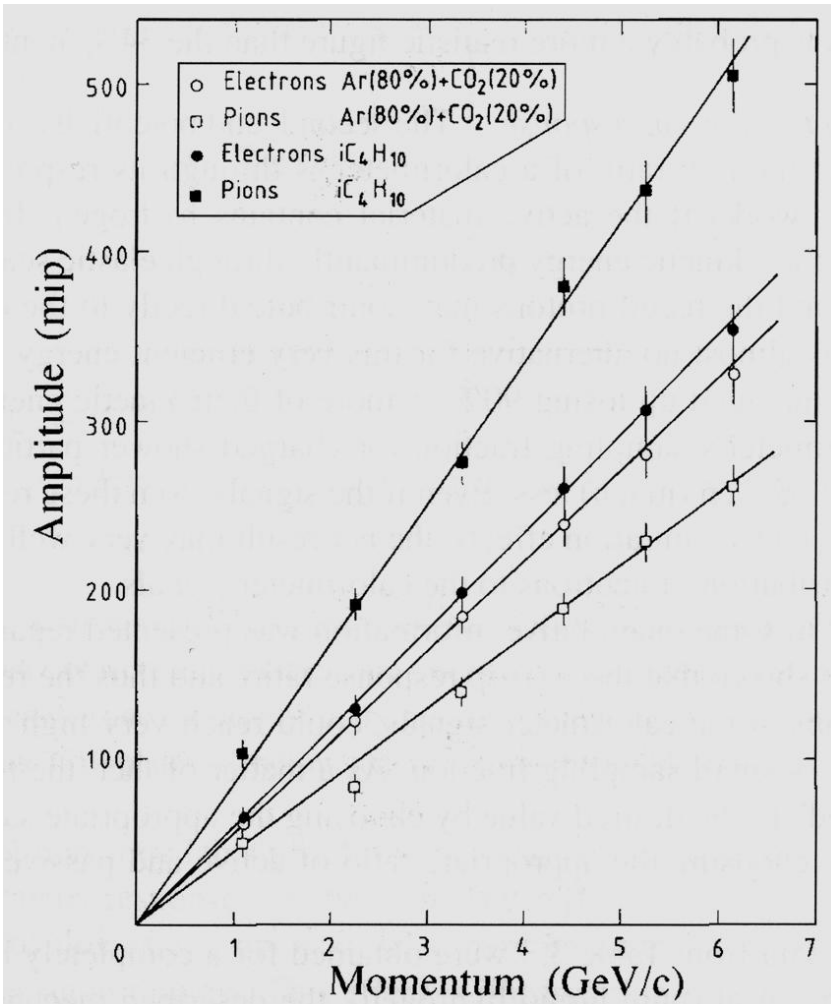
# Boosting the non-em response

- Mechanism: nuclear fission
  - Fission processes in non-em part of the shower development
    - => extra energy → nuclear  $\gamma$ S and soft evaporation neutrons
    - => Use depleted uranium  $^{238}\text{U}$
- Compensate to some extent for invisible energy ( $\approx 1/3$ )
- Nuclear fission neutrons increase  $f_n$ .
  - => n/mip value required for compensation is smaller than in the absence of fission neutrons.

# Boosting the non-em response (2)

- Manipulating the response to neutrons → active material has to contain hydrogen
    - Loss of kinetic energy of soft neutrons through elastic scattering with the hydrogen nuclei
    - Recoil protons → direct contribution to calorimeter signal.
    - Very efficient process → large contribution of neutrons to signal though possible saturation effect
  - Rule: The smaller the sampling fraction for charged particles, the larger the relative contribution of neutrons to the calorimeter signal.
- ⇒ Tuning of n/mip by choosing the appropriate sampling fraction for mips

# Boosting the non-em response (3)



- L3 Collaboration (LEP, CERN)
  - 2 gas mixtures: Ar/CO<sub>2</sub> and isobutane (iC<sub>4</sub>H<sub>10</sub>)
  - Electron signals barely affected by gas change
  - Pion signal increased by almost factor 2.
  - Ar/CO<sub>2</sub>: undercompensation (e/h~1.3)
  - Isobutane: Overcompensation (e/h~0.6)
- For compensation: Choose right gas mixture

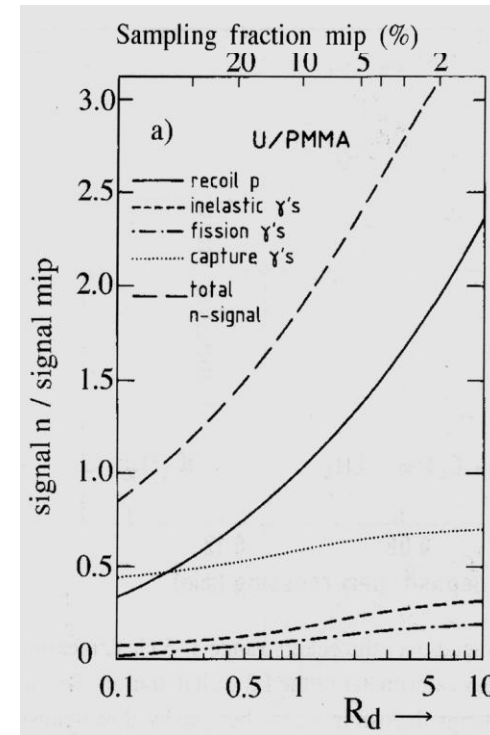
# Boosting the non-em response (4)

- In dense hydrogenous materials (plastic scintillators), e.g.  $^{238}\text{U}/\text{PMMA}$   
→ Saturation effects and higher densities

- Parameter  $R_d$ :

$$R_d = \frac{\text{thickness of passive material}}{\text{thickness of active material}}$$

- Monte Carlo Simulations:  $n/\text{mip}$  and  $e/h$  as function of  $R_d$



- Dominant contribution: recoil protons  
→ strongly dependent on sampling fraction

# Sampling fractions in different materials

- Uranium/plastic scintillator calorimeters:
  - Sampling fraction for compensation: 10%
- Lead calorimeter Pb/PMMA:
  - Sampling fraction for compensation: 3%
  - Differences to uranium:  
no fission processes → no neutron induced fission  $\gamma$ s and less neutrons → smaller value of  $f_n$   
larger e/mip value due to Z dependence of e/mip
- Low-Z absorber materials (copper, iron):
  - Even smaller sampling fraction for compensation
- Saturation: If saturation was absent, compensation would be achieved for much larger sampling fractions.

# Off-line compensation

- Determine energy sharing between em and non-em components of hadron showers on an event-to-event basis
- Apply weight factor  $e/h$  to the portion of the signal generated by the non-em components
- 2 methods:
  - Different spatial developments of em and non-em showers, especially in high- $Z$  absorber materials  $\rightarrow$  disentangle contributions of the 2 types of components
  - em showers  $\rightarrow$  electrons and positrons  $\rightarrow$  relativistic;  
non-em shower component  $\rightarrow$  spallation protons, recoil protons (not relativistic)  
 $\Rightarrow$  Comparison of Čerenkov and scintillation light produced in optical calorimeters





# Thanks for your attention

Literature:

Wigmans, R., *Calorimetry*, Oxford 2000, chap. 3.3

Figures:

Wigmans, R., *Calorimetry*, Oxford 2000, chap. 3.3

# e/h value in dependence of sampling fraction

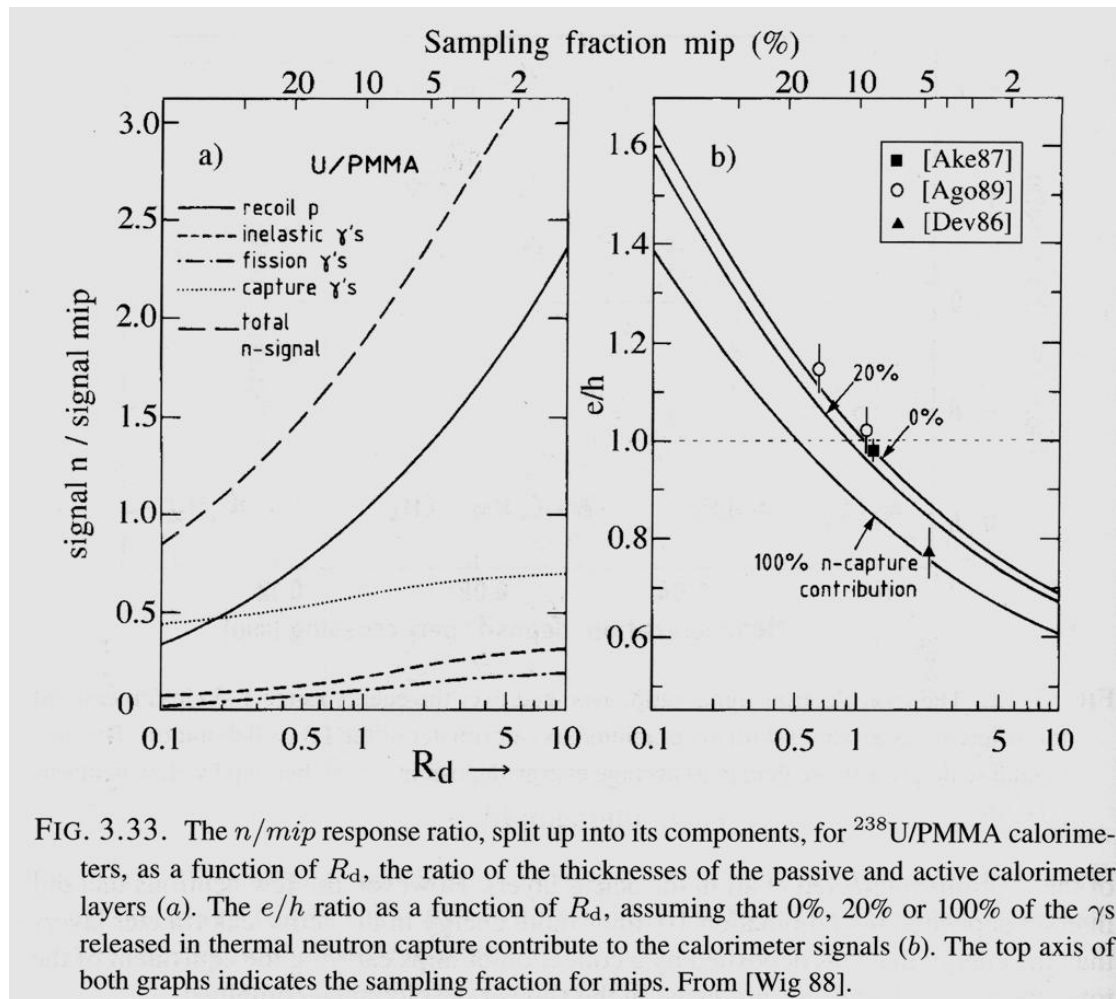


FIG. 3.33. The  $n/mip$  response ratio, split up into its components, for  $^{238}\text{U}/\text{PMMA}$  calorimeters, as a function of  $R_d$ , the ratio of the thicknesses of the passive and active calorimeter layers (a). The  $e/h$  ratio as a function of  $R_d$ , assuming that 0%, 20% or 100% of the  $\gamma$ s released in thermal neutron capture contribute to the calorimeter signals (b). The top axis of both graphs indicates the sampling fraction for mips. From [Wig 88].